

## Beam design example 2 - Glued laminated timber

Design a Glulam floor beam, simply supported, spanning 6.0m with uniformly distributed loads  
 Beam supporting floor joists @ 450crs

Dead load  $G = 1$  kN/m  
 Live load  $Q = 2.9$  kN/m

Load combinations from AS1170.0

Strength limit state:

$1.35G = 1.4$  kN/m  
 $1.2G+1.5Q = 5.6$  kN/m

Serviceability limit state:

$G + \psi_s Q = 3.03$  kN/m short term deflection where  $\psi_s = 0.7$   
 $G + \psi_l Q = 2.16$  kN/m long term deflection  $\psi_l = 0.4$

Using GL grades from AS/NZS 1328.2

Try 360x90 GL10 Glulam beam, using 45mm laminations

$d = 360$   $b = 90$

Check bending strength (NZS3603 3.2.4)

Design strength:

$\phi M_n = \phi k_1 k_4 k_5 k_6 k_8 k_{24} f_b Z$  for Glulam  
 $\phi = 0.8$   
 $k_1 = 0.6$  for a permanent load or 0.8 for medium term load  
 $k_4 = 1.0$  taken as 1.0 for GL grades  
 $k_5 = 1.0$  taken as 1.0 for GL grades  
 $L_{ay} = 450$  mm distance between restraints  
 $S = 1.35 (L_{ay} / b ((d/b)^2 - 1)^{0.5})^{0.5} = 5.94$  (or use Fig 3.1)  
 $k_8 = 1.0$  from NZS3603 Table 2.8  
 $f_b = 22.0$  MPa for GL10 from AS/NZS 1328.2 Table 1.2  
 $Z = bd^2/6 = 1944000$  mm<sup>3</sup>  
 $\phi M_{n long} = 20.5$  kNm for long term loading (permanent)  
 $\phi M_{n med} = 27.4$  kNm for medium term loading

Compare with design load

$M^*_{1.35G} = 6.1$  kNm <  $\phi M_{n long} = 20.5$  OK  
 $M^*_{1.2G+1.5Q} = 25.0$  kNm <  $\phi M_{n med} = 27.4$  OK

Check shear strength (NZS3603 3.2.3)

Design strength:

$\phi V_n = \phi k_1 k_4 k_5 f_s A_s$   
 $\phi, k_1, k_4, k_5$  factors from above  
 $f_s = 3.7$  MPa for GL10 from AS/NZS 1328.2 Table 1.2  
 $A_s = \frac{2}{3}bd = 43200$  mm<sup>2</sup>  
 $\phi V_{n long} = 76.7$  kN for long term loading (permanent)  
 $\phi V_{n med} = 102.3$  kN for medium term loading

Compare with design load

$V^*_{1.35G} = 4.1$  kN <  $\phi V_{n long} = 76.7$  OK  
 $V^*_{1.2G+1.5Q} = 16.7$  kN <  $\phi V_{n med} = 102.3$  OK

Check bearing strength (NZS3603 3.2.9)

assume bearing on 100mm wide top plate

Design strength:

$\phi N_{nbp} = \phi k_1 k_3 f_p A_p$

$k_1$	from above					
$k_3 =$	1.06					
$f_p =$	8.9	MPa		using MSG8 value, from NZS3603 Amendment 4, Table 2.3		
$A_p =$	13500	mm <sup>2</sup>		bearing area		
$\phi N_{nbp \text{ long}} =$	61.1	kN				
$\phi N_{nbp \text{ med}} =$	81.5	kN				
$N^*_{1.35G} =$	4.1	kN	<	$\phi N_{nbp \text{ long}} =$	61.1	OK
$N^*_{1.2G+1.5Q} =$	16.7	kN	<	$\phi N_{nbp \text{ med}} =$	81.5	OK

Check serviceability design limit state

$E =$	10.0	GPa		for GL10 from AS/NZS 1328.2 Table 1.2		
The lower bound modulus of elasticity, NZS3603 A4 doesn't need to be considered for Glulam						
$\Delta_G =$	4.8	mm		instantaneous dead load deflection		
$\Delta_Q =$	14.0	mm		instantaneous live load deflection		
$k_2 =$	1.5			creep factor for Glulam NZS3603 8.7.4		
$\Delta_{G+\psi_s Q} =$	14.6	mm		Span/400=	15 mm	OK
$\Delta_{k2(G+\psi_l Q)} =$	15.6	mm		Span/250=	24 mm	OK

refer to AS/NZS 1170.0 Table C1 for suggested serviceability limits

need to make a judgement call on the expected actual long term live load, the standard says 40% of live load ( $\psi_l = 0.4$ ), but probably 25% of the live load would be more accurate for a domestic situation ( $\psi_l = 0.25$ )

using $\psi_l =$	0.25		
$\Delta_{k2(G+\psi_l Q)} =$	12.5	mm	
Camber =	12.0	mm	

**use 360 x 90 GL10 Glulam, camber 12mm**